## DAIKIN

## technical data

## 

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## 1 Selection procedure VRVII system based on cooling load

## 1-1 Indoor unit selection

Enter indoor unit capacity tables at given indoor and outdoor temperature.
Select the unit that the capacity is the nearest to and higher than the given load.

## NOTE

1 Individual indoor unit capacity is subject to change by the combination. Actual capacity has to be calculated according to the combination by using outdoor units capacity table.

## 1-2 Outdoor unit selection

Allowable combinations are indicated in indoor unit combination total capacity index table.
In general, oudoor units can be selected as follows though the location of the unit, zoning and usage of the rooms should be considered.
The indoor and outdoor unit combination is determined that the sum of indoor unit capacity index is nearest to and smaller than the capacity index at $100 \%$ combination ratio of each outdoor unit. Up to 16 indoor units can be connected to one outdoor unit. It is recommended to choose a larger outdoor unit if the installation space is large enough.
If the combination ratio is higher than $100 \%$, the indoor unit selection will have to be reviewed by using actual capacity of each indoor unit.

Indoor unit combination total capacity index table

| Outdoor unit | Indoor unit combination ratio |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $130 \%$ | 120 \% | 110 \% | 100\% | 90\% | 80\% | 70\% | $60 \%$ | $50 \%$ |
| RXMO5M | 162.5 | 150 | 137.5 | 125 | 112.5 | 100 | 87.5 | 75 | 62.5 |
| RXM)Q8M/REYQ8M | 260 | 240 | 220 | 200 | 180 | 160 | 140 | 120 | 100 |
| RX(MQ10M/REYQ10M | 325 | 300 | 275 | 250 | 225 | 200 | 175 | 150 | 125 |
| RXYQ12M/REYQ12M | 390 | 360 | 330 | 300 | 270 | 240 | 210 | 180 | 150 |
| RXYQ14M/REYQ14M | 455 | 420 | 385 | 350 | 315 | 280 | 245 | 210 | 175 |
| RXYQ16M/REYQ16M | 520 | 480 | 440 | 400 | 360 | 320 | 280 | 240 | 200 |
| RXYQ18M/REYQ18M | 585 | 540 | 495 | 450 | 405 | 360 | 315 | 270 | 225 |
| RXYQ20M/REYQ20M | 650 | 600 | 550 | 500 | 450 | 400 | 350 | 300 | 250 |
| RXYQ22M/REYQ22M | 715 | 660 | 605 | 550 | 495 | 440 | 385 | 330 | 275 |
| RXYQ24M/REYQ24M | 780 | 720 | 660 | 600 | 540 | 480 | 420 | 360 | 300 |
| RXYQ26MMRYQ26M | 845 | 780 | 715 | 650 | 585 | 520 | 455 | 390 | 325 |
| RXYQ28M/REYQ28M | 910 | 840 | 770 | 700 | 630 | 560 | 490 | 420 | 350 |
| RXYQ30M/REYQ30M | 975 | 900 | 825 | 750 | 675 | 600 | 525 | 450 | 375 |
| RXYQ32M/REYQ32M | 1,040 | 960 | 880 | 800 | 720 | 640 | 560 | 480 | 400 |
| RXYQ34MMEYQ34M | 1,105 | 1,020 | 935 | 850 | 765 | 680 | 595 | 510 | 425 |
| RXYQ36M/REYQ36M | 1,170 | 1,080 | 990 | 900 | 810 | 720 | 630 | 540 | 450 |
| RXYQ38M/REYQ38M | 1,235 | 1,140 | 1,045 | 950 | 855 | 760 | 665 | 570 | 475 |
| RXYQ40MMREYQ40M | 1,300 | 1,200 | 1,100 | 1,000 | 900 | 800 | 700 | 600 | 500 |
| RXYQ42M/REYQ42M | 1,365 | 1,260 | 1,155 | 1,050 | 945 | 840 | 735 | 630 | 525 |
| RXYQ44MMEYQ44M | 1,430 | 1,320 | 1,210 | 1,100 | 990 | 880 | 770 | 660 | 550 |
| RXYQ46MMREYQ46M | 1,495 | 1,380 | 1,265 | 1,150 | 1,035 | 920 | 805 | 690 | 575 |
| RXYQ48M/REYQ48M | 1,560 | 1,440 | 1,320 | 1,200 | 1,080 | 960 | 840 | 720 | 600 |

Indoor unit capacity index

| Model | 20 | 25 | 32 | 40 | 50 | 63 | 80 | 100 | 125 | 200 | 250 |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity index | 20 | 25 | 31.25 | 40 | 50 | 62.5 | 80 | 100 | 125 | 200 | 250 |

## 1 Selection procedure VRVII system based on cooling load

## 1-3 Actual performance data

Use outdoor unit capacity tables
Determine the correct table according to the outdoor unit model and combination ratio.
Enter the table at given indoor and outdoor temperature and find the outdoor capacity and power input. The individual indoor unit capacity (power input) can be calculated as follows:
ICA $=\frac{\text { OCA } \times \operatorname{INX}}{\text { TNX }}$
TNX
ICA: Individual indoor unit capacity (power input)
OCA: Outdoor unit capacity (power input)
INX: Individual indoor unit capacity index
TNX: Total capacity index

Then, correct the indoor unit capacity according to the piping length.
If the corrected capacity is smaller than the load, the size of indoor unit has to be increased. Repeat the same selection procedure.

## 1-4 Selection example based on cooling load

1 Given

- Design condition

Cooling: indoor $20^{\circ} \mathrm{CWB}$, outdoor $33^{\circ} \mathrm{CDB}$

- Cooling load

| Room | A | B | C | D | $E$ | F | G | H |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load (kM | 2.9 | 2.7 | 2.5 | 4.3 | 4.0 | 4.0 | 3.9 | 4.2 |

- Power supply: 3-phase $380 \mathrm{~V} / 50 \mathrm{~Hz}$

2 Indoor unit selection
Enter indoor unit capacity table at:
20 CWB indoor temperature
33 CDB outdoor air temperature.
Selection results are as follows:

| Room | A | B | C | D | $E$ | F | G | H |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load (kW | 2.9 | 2.7 | 2.5 | 4.3 | 4.0 | 4.0 | 3.9 | 4.2 |
| Unit size | 25 | 25 | 25 | 40 | 40 | 40 | 40 |  |
| Capacity | 3.0 | 3.0 | 3.0 | 4.8 | 4.8 | 4.8 | 4.8 |  |

## 3 Outdoor unit selection

- Assume that the indoor and outdoor unit combination is as follows.

Outdoor unit: RXYQ10M
Indoor unit: FXCQ25M7 x 3, FXCQ40M7 x 5

- Indoor unit combination total capacity index $25 \times 3+40 \times 5=275(110 \%)$


## 1 Selection procedure VRVII system based on cooling load

## 1-4 Selection example based on cooling load

4 Actual performance data ( 50 Hz )

- Outdoor unit cooling capacity: 30.5kW (RXYQ10M, $110 \%$ )
- Individual capacity

Capacity of FXYCP25K $=30.5 \times \frac{25}{275}=2.77 \mathrm{~kW}$
Capacity of FXYCP40K7 $=30.5 \times \frac{40}{275}=4.44 \mathrm{~kW}$
Actual combination capacity

| Room | A | B | C | D | E | F | G | H |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load (kW) | 2.9 | 2.7 | 2.5 | 4.3 | 4.0 | 4.0 | 3.9 | 4.2 |
| Unit size | 25 | 25 | 25 | 40 | 40 | 40 | 40 | 40 |
| Capacity | 2.77 | 2.77 | 2.77 | 4.44 | 4.44 | 4.44 | 4.44 | 4.44 |

The unit size for room A has to be increased from 25 to 32 because the capacity is less than the load. For new combination, actual capacity is calculated as follows.

- Indoor unit combination total capacity index $(25 \times 2)+31.25+(40 \times 5)=281.25(112.5 \%)$
- Outdoor unit cooling capacity:
$27,610 \mathrm{kcal} / \mathrm{h}$ (direct interpolation between $110 \%$ and $120 \%$ in the table)
- Individual capacity

| Capacity of FXCQ25M | $=30.0 \times \frac{25}{281.25}=2.7 \mathrm{~kW}$ |
| :--- | :--- |
| Capacity of FXCQ32M | $=30.0 \times \frac{32}{281.25}=3.4 \mathrm{~kW}$ |
| Capacity of FXCQ40M | $=30.0 \times \frac{40}{281.25}=4.3 \mathrm{~kW}$ |

Actual capacity of new combination

| Room | A | B | C | D | E | F | G |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load (KW) | 2.9 | 2.7 | 2.5 | 4.3 | 4.0 | 4.0 | 3.9 | 4.2 |
| Unit size | 32 | 25 | 25 | 40 | 40 | 40 | 40 |  |
| Capacity | 3.4 | 2.7 | 2.7 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 |

Then, the capacities have to be corrected for actual piping length according to the location of indoor and outdoor units and the distance between them.

## 2 Capacity correction ratio

## 2-1 RX(Y)Q5M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity = cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXM)05M | 019.1 | not increased |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size

| Rate of change <br> (object piping) | Correction factor |  |
| :---: | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | 0.5 |
| Heating (liquid pipe) | 1.0 | - |

Example


In the above case
(Cooling) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
(Heating) Overall equivalent length $=80 \mathrm{~m} \times 1.0+40 \mathrm{~m}=120 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.78 heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 1.0

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position $H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length ( m )
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | gas | liquid |
| :---: | :---: | :---: |
| RXMM55M | $\varnothing 15.9$ | 09.5 |

## 2 Capacity correction ratio

## 2-2 RX(Y)Q8M, RXYQ22M

- Rate of change in cooling capacity

- Rate of change in heating capacity


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## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $x$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXX)Q8M | $\varnothing 22.2$ | $\varnothing 12.7$ |
| RXYQ22M | $\varnothing 31.8$ | $\varnothing 19.1$ |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size

| Rate of change <br> (object piping) | Correction factor |  |
| :---: | :---: | :---: |
|  | Standard size | Size increase |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
(Heating) Overall equivalent length $=80 \mathrm{~m} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.86
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 1.0

EXPLANATION OF SYMBOLS
$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position $H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | gas | liquid |
| :--- | :---: | :---: |
| RX(M)Q8M | $\varnothing 19.1$ | 09.5 |
| RXYQ22M | $\varnothing 28.6$ | $\varnothing 15.9$ |

## 2 Capacity correction ratio

## 2-3 RX(Y)Q10M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit)
cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change
When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is:
cooling / heating capacity $=$ cooling / heating capacity of each unit $\times$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased.
Diameter of above case

| Model | gas | liquid |
| :---: | :---: | :---: |
| RXMOQ10M | $\oplus 25.4$ | $\oplus 12.7$ |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size.

| Rate or change <br> (object piping) | Correction factor |  |
| :--- | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | 0.5 |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
(Heating) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.87
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.90

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference ( $m$ ) between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length ( m )
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | gas | liquid |
| :---: | :---: | :---: |
| RX(Y)Q10M | $\varnothing 22.2$ | $\varnothing 9.5$ |

## 2 Capacity correction ratio

## 2-4 RXYQ12,14,24,36M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions. Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=\underline{\text { cooling / heating capacity obtained from performance characteristics table } x \text { each capacity rate of change }}$ When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main liquid pipes (outdoor unit-branch sections) must be increased.
Diameter of above case

| Model | gas | liquid |
| :---: | :---: | :---: |
| RXYQ12,14M | Not Increased | 015.9 |
| RXYQ24M |  | 019.1 |
| RXYQ36M |  | 022.2 |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
$\underline{\text { Overall equivalent length }}=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size.

| Rate or change <br> (object piping) | Correction factor |  |
| :--- | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | - |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=80 \mathrm{~m} \times 1.0+40 \mathrm{~m}=120 \mathrm{~m}$
(Heating) Overall equivalent length $=80 \mathrm{~m} \times 0.5+40 \mathrm{~m}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.88
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 1.0
EXPLANATION OF SYMBOLS
$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position $H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ12,14M | $\varnothing 28.6$ | $\varnothing 12.7$ |
| RXYQ24M | $\varnothing 34.9$ | $\varnothing 15.9$ |
| RXYQ36M | $\varnothing 41.3$ | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-5 RXYQ16M

- Rate of change in cooling capacity




## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit)
cooling / heating capacity = cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change
When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is:
cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ16M | $\varnothing 31.8$ | 015.9 |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size.

| Rate or change <br> (object piping) | Correction factor |  |
| :--- | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | 0.5 |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=80 \mathrm{~m} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
(Heating) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+40 \mathrm{~m}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.88
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 1.0

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of pipes

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ16M | $\varnothing 28.6$ | $\varnothing 12.7$ |

## 2 Capacity correction ratio

## 2-6 RXYQ18,26,28,30,38,40,42,44M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions. Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity = cooling / heating capacity obtained from performance characteristics table $x$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is:
cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased except for the gas pipe of $R X(Y) Q 38,40,42,44 M$.
Diameter of above case

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ18M | $\varnothing 31.8$ | $\varnothing 19.1$ |
| RXYQ26,28,30M | $\varnothing 38.1$ | $\varnothing 22.2$ |
| RXYQ38,40,42,44M | Not Increased | $\varnothing 22.2$ |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size.

| Rate or change <br> (object piping) | Correction factor |  |
| :--- | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | 0.5 |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{1.0}+\underline{40 \mathrm{~m}}=120 \mathrm{~m}$
(Heating) Overall equivalent length $=80 \mathrm{~m} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.83
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 1.0

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXQ18M | $\varnothing 28.6$ | $\varnothing 15.9$ |
| RXYQ26,28,30M | $\varnothing 34.9$ | $\varnothing 19.1$ |
| RXYQ40,42,44M | $\varnothing 41.3$ | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-7 RXYQ20,32,34,46M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $x$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased except for the gas pipe of $\mathrm{RX}(\mathrm{Y}) \mathrm{Q} 46 \mathrm{M}$.
Diameter of above case

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ20M | $\varnothing 31.8$ | $\varnothing 19.1$ |
| RXYQ32,34M | $\varnothing 38.1$ | $\varnothing 22.2$ |
| RXYQ46M | Not Increased | $\varnothing 22.2$ |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size.

| Rate or change <br> (object piping) | Correction factor |  |
| :--- | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | 0.5 |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=80 \mathrm{~m} \times 1.0+40 \mathrm{~m}=120 \mathrm{~m}$
(Heating) Overall equivalent length $=80 \mathrm{~m} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.82
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 1.0

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference ( $m$ ) between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor
Diameter of gas pipes

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ18M | $\varnothing 28.6$ | $\varnothing 15.9$ |
| RXYQ26,28,30M | $\varnothing 34.9$ | $\varnothing 19.1$ |
| RXYQ40,42,44M | $\varnothing 41.3$ | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-8 RXYQ48M

- Rate of change in cooling capacity

2


- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | liquid | gas |
| :--- | :---: | :---: |
| RXYQ48M | $\emptyset 22.2$ | not increased |

5 Read cooling / heating capacity rate of change in the above figures based on the following equivalent length.
Overall equivalent length $=$ Equivalent length to main pipe $\times$ Correction factor + Equivalent length after branching
Choose a correction factor from the following table.
When cooling capacity is calculated: gas pipe size
When heating capacity is calculated: liquid pipe size.

| Rate or change <br> (object piping) | Correction factor |  |
| :--- | :---: | :---: |
|  | Standard size | Size increase |
| Cooling (gas pipe) | 1.0 | - |
| Heating (liquid pipe) | 1.0 | 0.5 |

Example


In the above case
(Cooling) Overall equivalent length $=80 \mathrm{~m} \times 1.0+40 \mathrm{~m}=120 \mathrm{~m}$
(Heating) Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity in cooling capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.82
heating capacity when $\mathrm{Hp}=0 \mathrm{~m}$ is thus approximately 0.97

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length ( m )
$\alpha$ : Capacity correction factor

Diameter of pipes

| Model | gas | liquid |
| :--- | :---: | :---: |
| RXYQ48M | $\varnothing 41.3$ | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-9 REYQ8,22M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit)
cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $\times$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas pipes (outdoor unit-branch sections) must be increased.
Diameter of above case

| Model | Liquid |
| :--- | :---: |
| REYQ8M | 012.7 |
| REYQ22M | $\varnothing 19.1$ |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) Overall equivalent length $=$ Equivalent length to main pipe $\times 0.5+$ Equivalent length after branching Example


In the above case (Heating)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 1.0
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity.
$\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe }} \times \underline{0.5}+\underline{\text { Equivalent length after branching }}$
Example


In the above case (Cooling)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.86

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of pipes

| Model | liquid |
| :--- | :---: |
| REYQ8M | $\varnothing 9.5$ |
| REYQ22M | $\varnothing 15.9$ |

## 2 Capacity correction ratio

## 2-10 REYQ10M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | liquid |
| :--- | :---: |
| REYQ10M | $\emptyset 12.7$ |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) Overall equivalent length $=$ Equivalent length to main pipe $\times \underline{0.5}+$ Equivalent length after branching
Example


In the above case (Heating)
Overall equivalent length $=80 \mathrm{~m} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.91
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity.
$\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe } \times 0.5+\text { Equivalent length after branching }}$
Example


In the above case (Cooling)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.88

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length ( m )
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | liquid |
| :--- | :---: |
| REYQ10M | 09.5 |

## 2 Capacity correction ratio

## 2-11 REYQ12,14,24,36M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity = cooling / heating capacity obtained from performance characteristics table $x$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | liquid |
| :--- | :---: |
| REYQ12,14M | $\varnothing 15.9$ |
| REYQ24M | $\varnothing 19.1$ |
| REYQ36M | $\varnothing 22.2$ |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) $\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe } \times 0.5+\text { Equivalent length after branching }}$ Example


In the above case (Heating)
$\underline{\text { Overall equivalent length }}=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 1.0
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity. $\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe }} \times \underline{0.5}+$ Equivalent length after branching Example


In the above case (Cooling)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.92

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference ( $m$ ) between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | liquid |
| :--- | :---: |
| REYQ12,14M | $\varnothing 12.7$ |
| REYQ24M | $\varnothing 15.9$ |
| REYQ36M | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-12 REYQ16M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $x$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | liquid |
| :--- | :---: |
| REYQ16M | $\emptyset 15.9$ |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) $\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe } \times 0.5+\text { Equivalent length after branching }}$
Example


In the above case (Heating)
Overall equivalent length $=80 \mathrm{~m} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 1.0
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity.
$\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe } \times \underline{0.5}+\text { Equivalent length after branching }}$
Example


In the above case (Cooling)
$\underline{\text { Overall equivalent length }}=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.88

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference ( $m$ ) between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length ( m )
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | liquid |
| :--- | :---: |
| REYQ16M | $\varnothing 12.7$ |

## 2 Capacity correction ratio

## 2-13 REYQ18,26,28,30,38,40,42,44M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit)
cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change
When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is:
cooling / heating capacity $=$ cooling / heating capacity of each unit $\times$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased.
Diameter of above case

| Model | liquid |
| :--- | :---: |
| REYQ18M | $\varnothing 19.1$ |
| REYQ26,28,30,38,40,42,44M | $\varnothing 22.2$ |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) Overall equivalent length $=$ Equivalent length to main pipe $\times \underline{0.5}+\underline{\text { Equivalent length after branching }}$ Example


In the above case (Heating)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 1.0
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity.
$\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe }} \times \underline{0.5}+\underline{\text { Equivalent length after branching }}$
Example


In the above case (Cooling)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.88

## - EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference ( $m$ ) between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of pipes

| Model | liquid |
| :--- | :---: |
| REYQ18M | 015.9 |
| REYQ26,28,30,38,40,42,44M | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-14 REYQ20,32,34,46M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## | notes

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit) cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $x$ each capacity rate of change When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is: cooling / heating capacity $=$ cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased. Diameter of above case

| Model | liquid |
| :--- | :---: |
| REYQ20M | $\propto 19.1$ |
| REYQ32,34,46M | $\varnothing 22.2$ |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) $\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe }} \times \underline{0.5}+\underline{\text { Equivalent length after branching }}$ Example


In the above case (Heating)
$\underline{\text { Overall equivalent length }}=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 1.0
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity.
Overall equivalent length $=$ Equivalent length to main pipe $\times \underline{0.5}+$ Equivalent length after branching
Example


In the above case (Cooling)
$\underline{\text { Overall equivalent length }}=\underline{80 \mathrm{~m}} \times \underline{0.5}+40 \mathrm{~m}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.87

## EXPLANATION OF SYMBOLS

$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length (m)
$\alpha$ : Capacity correction factor

Diameter of gas pipes

| Model | liquid |
| :--- | :---: |
| REYQ20M | $\varnothing 15.9$ |
| REYQ32,34,46M | $\varnothing 19.1$ |

## 2 Capacity correction ratio

## 2-15 REYQ48M

- Rate of change in cooling capacity

- Rate of change in heating capacity



## NOTES

1 These figures illustrate the rate of change in capacity of a standard indoor unit system at maximum load (with the thermostat set to maximum) under standard conditions.
Moreover, under partial load conditions there is only a minor deviation from the rate of change in capacity shown in the above figures.
2 With this outdoor unit, evaporating pressure constant control when cooling, and condensing pressure constant control when heating is carried out.
3 Method of calculating cooling / heating capacity (max. capacity for combination with standard indoor unit)
cooling / heating capacity $=$ cooling / heating capacity obtained from performance characteristics table $\times$ each capacity rate of change
When piping length differs depending on the indoor unit, maximum capacity of each unit during simultaneous operation is:
cooling / heating capacity = cooling / heating capacity of each unit $x$ capacity rate of change for each piping length
4 When overall equivalent pipe length is 90 m or more, the diameter of the main gas and liquid pipes (outdoor unit-branch sections) must be increased except for the gas pipe of $R X(Y) Q 46 M$.
Diameter of above case

| Model | liquid |
| :--- | :---: |
| REYQ48M | 022.2 |

5 When the main sections of the interunit gas pipe diameters are increased the overall equivalent length should be calculated as follows. (Heating only) Overall equivalent length $=$ Equivalent length to main pipe $\times \underline{0.5}+$ Equivalent length after branching
Example


In the above case (Heating)
$\underline{\text { Overall equivalent length }}=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.97
6 In the combination which does not include cooling only indoor unit, calculate the equivalent length pipe by the following when you calculate cooling capacity.
$\underline{\text { Overall equivalent length }}=\underline{\text { Equivalent length to main pipe }} \times \underline{0.5}+\underline{\text { Equivalent length after branching }}$
Example


In the above case (Cooling)
Overall equivalent length $=\underline{80 \mathrm{~m}} \times \underline{0.5}+\underline{40 \mathrm{~m}}=80 \mathrm{~m}$
The correction factor in capacity when $\mathrm{H}_{\mathrm{p}}=0 \mathrm{~m}$ is thus approximately 0.87

EXPLANATION OF SYMBOLS
$H_{p}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in inferior position
$H_{M}$ : Level difference $(m)$ between indoor and outdoor units with indoor unit in superior position
L : Equivalent pipe length ( m )
$\alpha$ : Capacity correction factor
Diameter of gas pipes

| Model | liquid |
| :--- | :---: |
| REYQ48M | $\varnothing 19.1$ |

## 3 Integrated heating capacity coefficient

1 The tables do not take account of the reduction in capacity when frost has accumulated or while the defrosting operation is in progress. The capacity values which take these factors into account, in other words the integrated heating capacity values, can be calculated as follows:

Formula: Integrated heating capacity = A
Value given in table of capacity characteristics $=B$
Integrating correction factor for frost accumulation (kW) $=\mathrm{C}$
$A=B \times C$
2 Correction factor for finding integrated heating capacity

| Inet port temperature of heat exchanger $\left({ }^{\circ} \mathrm{C} / \mathrm{RH} \mathrm{H5} \mathrm{\%}\right)$ | -7 | -5 | -3 | 0 | 3 | 5 | 7 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Integrating correction factor for frost accumulation | 0.96 | 0.93 | 0.87 | 0.81 | 0.83 | 0.89 | 1.0 |



NOTE

- The figure shows that the integrated heating capacity expresses the integrated heating capacity for a single cycle (from defrost operation to defrost operation) in terms of time.

3 Please note that when there is an accumulation of snow against the outside surface of the outdoor unit heat exchanger, there will always be a temporary reduction in capacity although this will, of course, vary in degree in accordance with a number of other factors such as the outdoor temperature ( CDB), relative humidity ( RH ) and the amount of frosting which occurs.

## 4 Refnet pipe system

## 4－1 Refnet joints

## 4－1－1 VRVII heat pump

|  | Liquid side junction | Suction gas side junction |  |
| :---: | :---: | :---: | :---: |
|  |  |  | $2 \times 8$ <br> （10） |
|  |  |  | $\begin{array}{r} (3) \\ 2 \times(4) \end{array}$ |
|  |  |  | $\begin{aligned} & \text { (3) } \\ & \text { (4) } \\ & \text { (2) } \\ & \text { (5) } \end{aligned}$ |
| $\begin{aligned} & \text { 华 } \\ & \text { 刘 } \\ & \text { 㸓 } \end{aligned}$ |  |  | （5）（2） <br> （6） <br> （10） $2 \times(14)$ |

## 4 Refnet pipe system

## 4-1 Refnet joints

## 4-1-2 VRVII heat recovery

|  | Liquid side junction | Discharge gas side junction | Suction gas side junction |
| :---: | :---: | :---: | :---: |
|  |  |  | (10) |
|  |  |  |  |
|  |  |  |  |
|  |  | (8)(2) |  |

## 4 Refnet pipe system

## 4－2 Refnet headers

## 4－2－1 VRVII heat pump

|  | Liquid side header | Suction gas side header |  |
| :---: | :---: | :---: | :---: |
| ㄷ⿳亠二口丿 文 푼 |  |  | $6 \times($ <br> （17） <br> （18） |
|  |  |  | $\begin{aligned} & 6 \times(C \\ & 2 \times(18 \end{aligned}$ |
|  |  |  | $\begin{aligned} & 6 \times(\square) \\ & 4 \times(10) \end{aligned}$ |

## 4－2－2 VRVII heat recovery

|  | Liquid side header | Discharge gas side header | Suction gas side header |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  | (1) |  |  |
|  |  |  | $5 \times(10)$ $6 \times \text { © }$ |

## 4 Refnet pipe system

## 4-3 Reducers, Expanders



## 4-4 Closed pipes

(A)

## 4 Refnet pipe system

## 4-5 Outdoor unit multi piping connection kit

## 4-5-1 VRVII heat pump

|  | Suction gas side junction | Liquid side juntion | Reduces/ / Expanders |  |  | Joint for ol pipe |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | For suction gas pipe | For discharge gas pipe | For liquid pipe |  |
|  |  |  |  |  |  |  |
| $\begin{aligned} & \text { M } \\ & \sum_{\text {N }}^{y} \\ & \text { 亭 } \end{aligned}$ |  |  |  |  |  |  |
|  |  |  | (3x) |  |  | 团 |

## 4 Refnet pipe system

4-5 Outdoor unit multi piping connection kit

## 4-5-2 VRVII heat recovery

|  | Suction ass side juntion | Dischare eas side jejurion | Liquid Sde jinction | Redices / Exandes |  |  | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Jint for oil } \\ \text { pipe } \end{array} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | For sction gas pipe | For distage ofa pipe | For liquid pipe |  |
| $\begin{aligned} & \text { 䯧 } \\ & \text { 窎 } \end{aligned}$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  | $(3 x)$ |  |  |  |

4 Refnet pipe system

## 4-6 Example of Refnet piping layouts



## 5 REFNET pipe selection

## 5-1 RX(Y)Q5-10M, RXYQ12-48M



## 5 REFNET pipe selection

## 5-2 REYQ8~48M




## 5-3 Piping thickness

| Piping diameter | Material | Minimum thickness [mm] |
| :---: | :---: | :---: |
| $\varnothing 6.4$ | 0 | 0.8 |
| $\varnothing 9.5$ | 0 | 0.8 |
| $\varnothing 12.7$ | 0 | 0.8 |
| $\varnothing 15.9$ | 0 | 0.99 |
| $\varnothing 19.1$ | $1 / 2 \mathrm{H}$ | 0.8 |
| $\varnothing 22.2$ | $1 / 2 \mathrm{H}$ | 0.8 |
| $\varnothing 28.6$ | $1 / 2 \mathrm{H}$ | 0.99 |
| $\varnothing 34.9$ | $1 / 2 \mathrm{H}$ | 1.21 |
| $\varnothing 41.3$ | $1 / 2 \mathrm{H}$ | 1.43 |

:O : annealed
$1 / 2 \mathrm{H}$ : half-hard
For half hard pipes the maximum allowed tensile stress is $61 \mathrm{~N} / \mathrm{mm}^{2}$. For this reason the $0.2 \%$ proof strength of the half hard pipe shall be minimum $61 \mathrm{~N} / \mathrm{mm}^{2}$.
The bending radius is more than or equal to 3 times the diameter of the pipe.

## 䉪墇III <br> Systems



ISO14001 assures an effective environmental management system in order to help protect human $h$ health•and the environment from the potential impact of our activities, products and services and to assist in maintaining and improving the quality of the environment.

Daikin Europe N.V. is approved by LRQA for its Quality Management System in accordance with the ISO9001 standard. ISO9001 pertains to quality assurance regarding design, development, manufacturing as well as to services
related to the product. related to the product

Daikin units comply with the European regulations that guarantee the safety of the product.

VRV products are not within the scope of the Eurovent certification programme.

Daikin equipment is designed for comfort applications. For use in other applications, please contact your local Daikin
representative.

